

The “beReal” Project

Scientific Highlights

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Providing **insights & highlights** of the **development process** of the „beReal“ methods for firewood and pellet stoves

Firewood Stoves*

- Suction pyrometer – Effect on (indirect) efficiency determination
- Thermal efficiency – Direct vs. indirect determination & the effect of cooling down
 - Effect of ignition mode on combustion performance
 - Effect of draught conditions on combustion performance

a) Tests from an accredited test institute (experiments of a previous project):

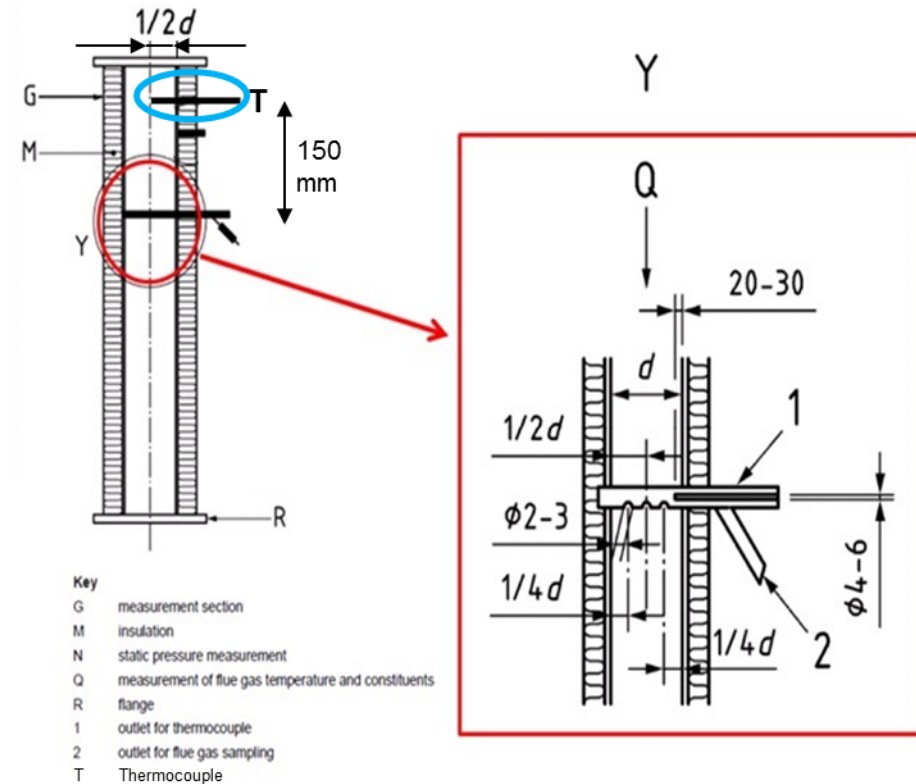
- 3 Roomheaters according to EN 13240 (A, B, C) → thermal efficiency (indirect)

$$\eta = 100 - (q_a + q_b + q_r)$$

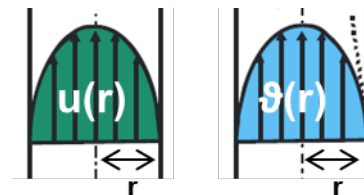
- Thermal (q_a) & chemical (q_b) flue gas losses & losses due to unburnt material (q_r)

b) Comparative combustion tests

- 1 Roomheater acc. to EN 13240
- Flue gas temperature measurement:
 - Suction pyrometer (different suction velocities)
 - Thermocouple (centrally placed in the flue gas pipe)
- Evaluation of measured temperature differences and their impact on indirect thermal efficiency determination
- Variation of flue gas velocities in the suction pyrometer

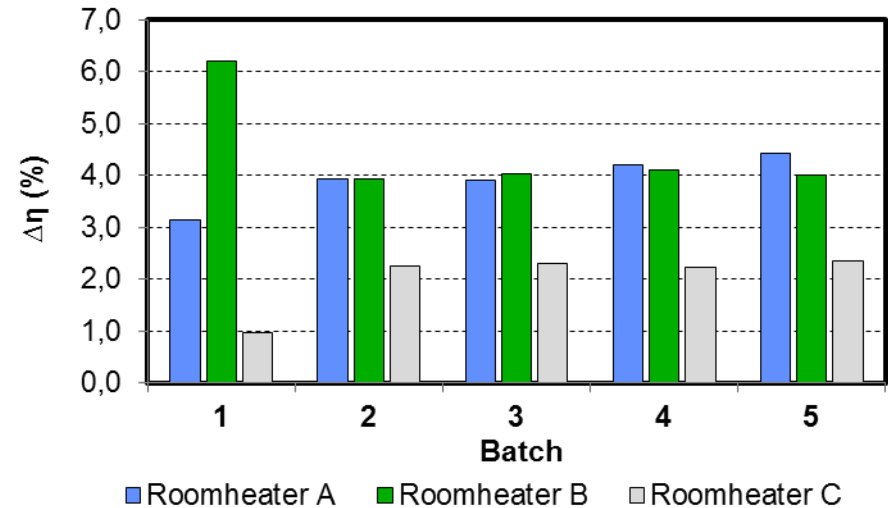
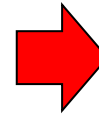
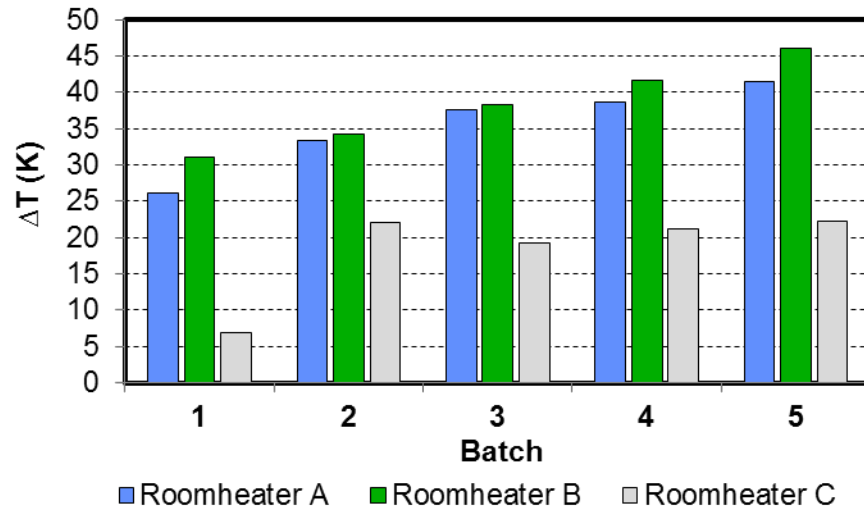


Source: EN 13240



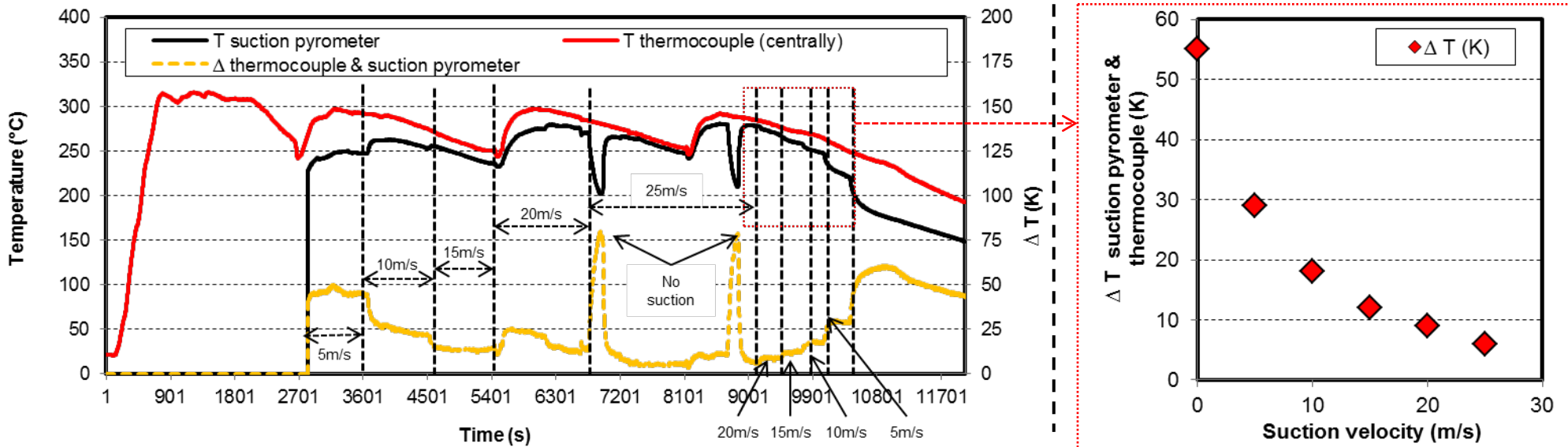
Velocity $u(r)$ and temperature $\vartheta(r)$ profile depend on flow conditions in the flue gas pipe

Results a) Tests from an accredited test institute (experiments of a previous project)



- **Clear differences** between suction pyrometer and core temperature (thermocouple) obvious (for all three tested roomheaters) → Higher temperatures measured with the thermocouple (**7K – 46K**)
 - Consequently differences of **thermal efficiencies** varied from **1 % to 6.2 % (Ø 3.5 %)**.
 - The required flue gas velocity in the suction pyrometer (20-25 m/s) is **not/ hardly** reached when only gas analyzers are used for flue gas suction.
- Flue gas temperature measurement is essential for thermal efficiency determination

Results b) Comparative combustion tests



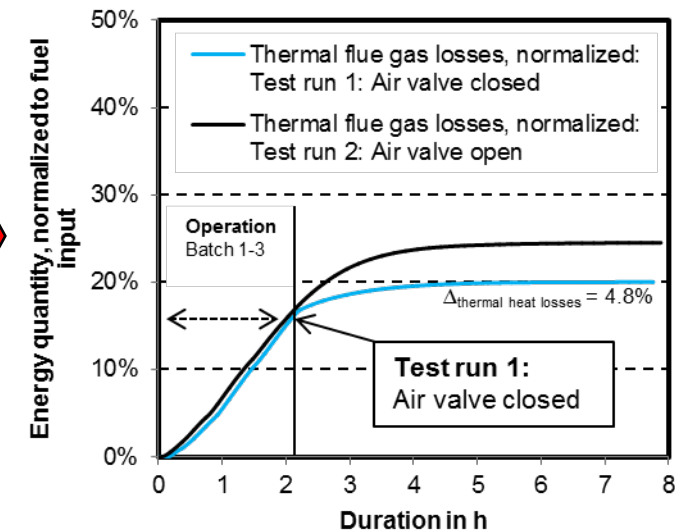
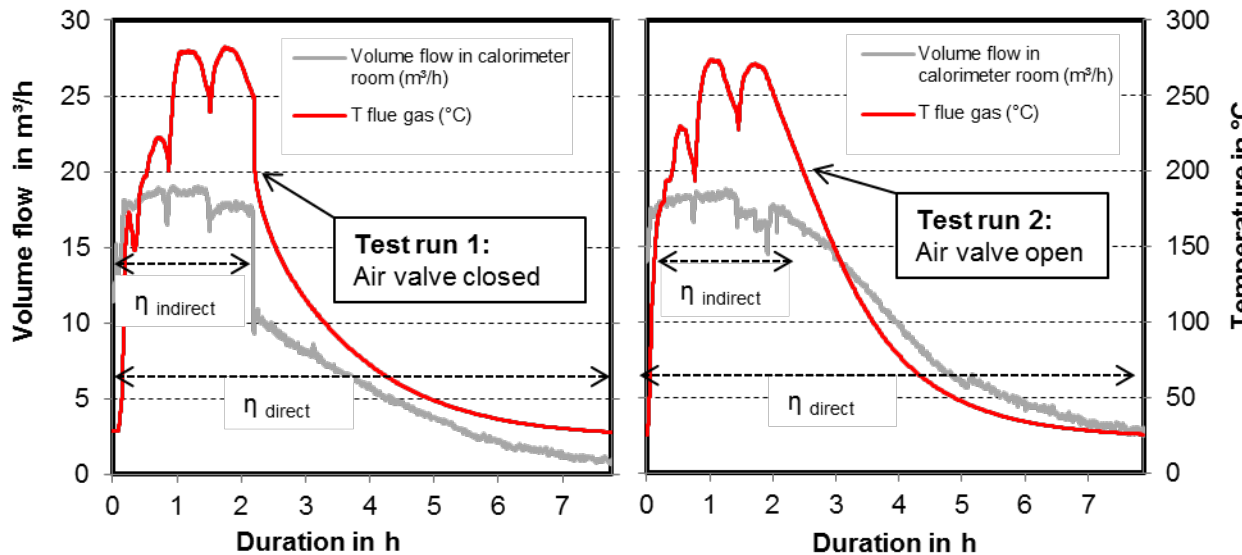
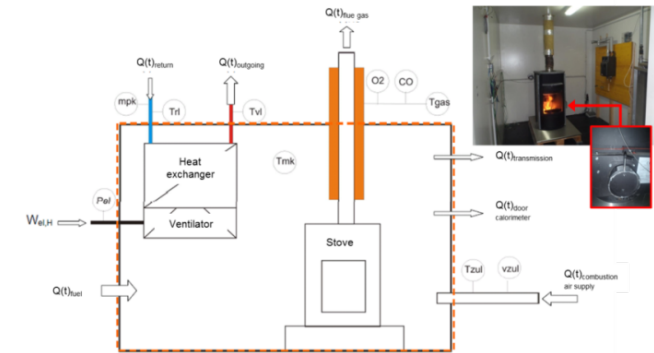
- Correlation of suction velocity and measured temperature with suction pyrometer clearly evident
- Highest impact of suction velocity on temperature difference between 0 to 15 m/s
- Differences between thermocouple and suction pyrometer was around 5 to 10 K (even when suction velocity was ≥ 20 m/s).
- Thermocouple measurement less error-prone compared to the suction pyrometer measurement
- Relevance for the beReal test method: Flue gas temperature measurement will be done with a thermocouple centrally placed in the flue gas pipe

Firewood Stoves

Thermal efficiency – Direct vs. indirect & the effect of cooling down

Approach

- Comparative assessment of thermal efficiency using the **indirect** (EN 13240) and **direct** (calorimeter room) approach
- Comparative test with a roomsealed roomheater (3 batches per test cycle)

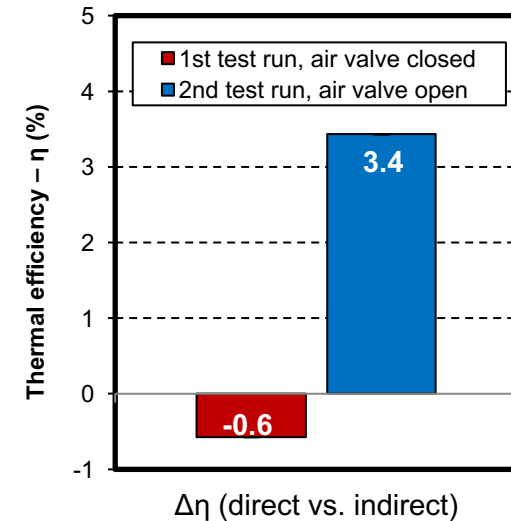
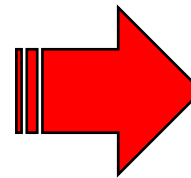
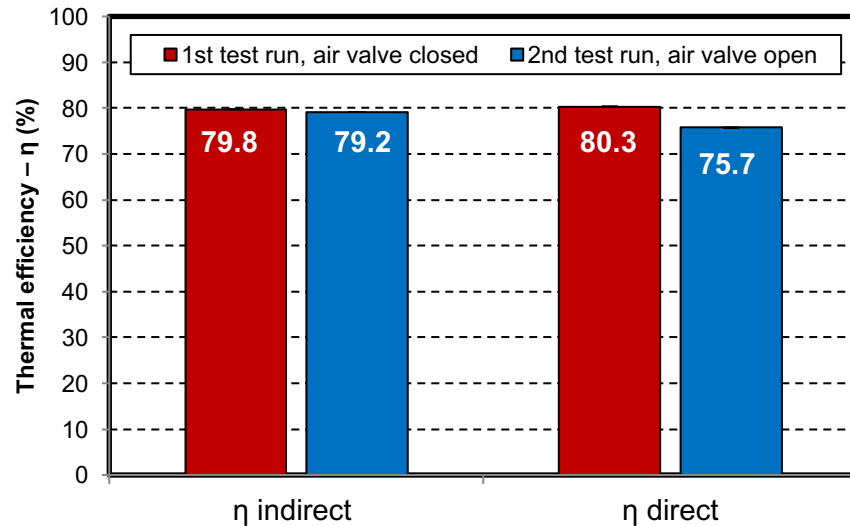


Results

- Cooling down process & air valve settings** after heating operation influence thermal efficiency performance → should be respected in the beReal test procedure
- Important aspect for avoiding emissions and low efficiency in real-life operation (**Quick-User-Guide!**)

$$\eta_{direct} = \frac{Output}{Input} = \frac{E_{Heat\ exchanger\ (kWh)} + E_{Transmission\ (kWh)} - E_{Ventilator\ (kWh)}}{E_{Fuel\ input\ (kWh)}} \times 100\%$$

$$\eta_{indirect\ EN13240} = (1 - thermal\ losses - chemical\ losses - 0.005) \times 100\%$$



Results:

Test-run 1: Air valve closed - after heating operation

- **Negligible differences** between direct and indirect efficiency determination

Test-run 2: Air valve open - after heating operation

- Higher differences of efficiency (direct vs. indirect)
- Reason: **Thermal losses of cool down phase** are not respected in the indirect efficiency determination process

Firewood Stoves

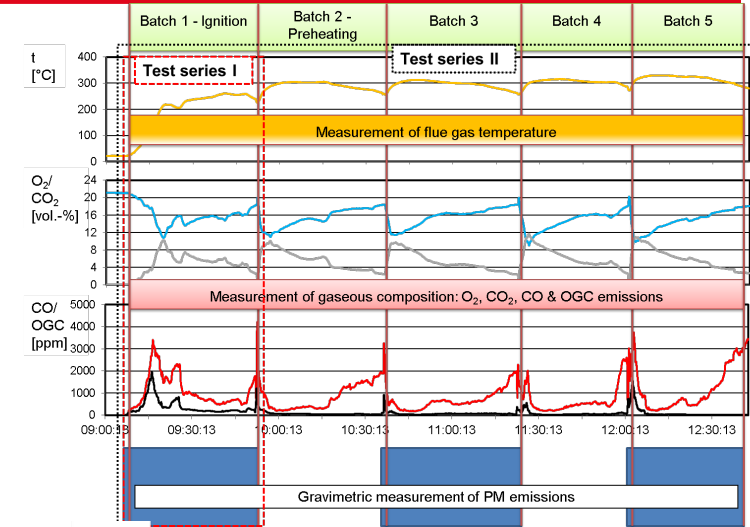
Effect of ignition mode and draught conditions

Approach

Ignition tests (Test series I)

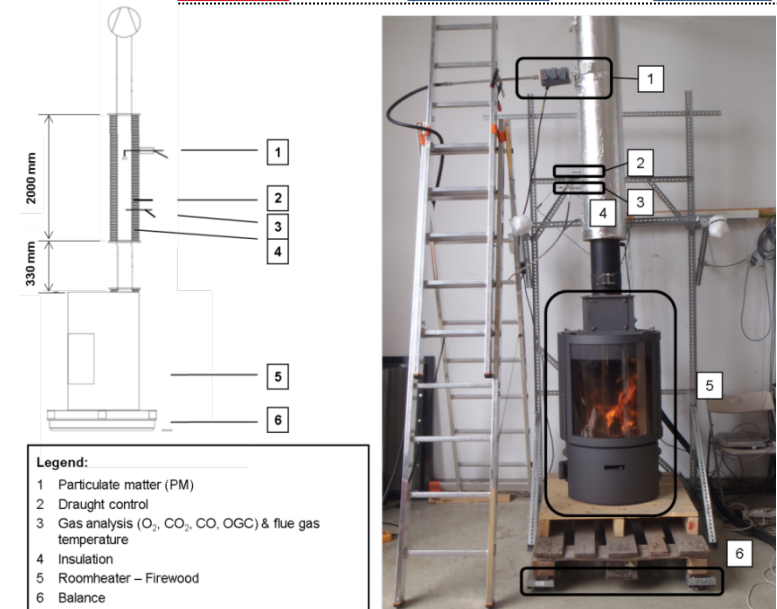
- Start from cold conditions
- Three test runs for each variation / two roomheaters (A, B)

Top-down ignition mode		Bottom-up ignition mode	
Variation 1	Variation 2	Variation 3	Variation 4
Spruce kindling (Spruce + Beech)	Beech kindling (Beech + Beech)	Spruce kindling (Spruce + Beech)	Beech kindling (Beech + Beech)



Effect Draught conditions (Test series II)

- One test cycle for each draught level – 12Pa, 24Pa, 48Pa
- 5 batches per test cycle with three roomheaters (A, B, D)



Firewood Stoves

Effect of ignition mode

Bottom-up vs. top-down

- Kindling material: Impact in general very low

Roomheater A:

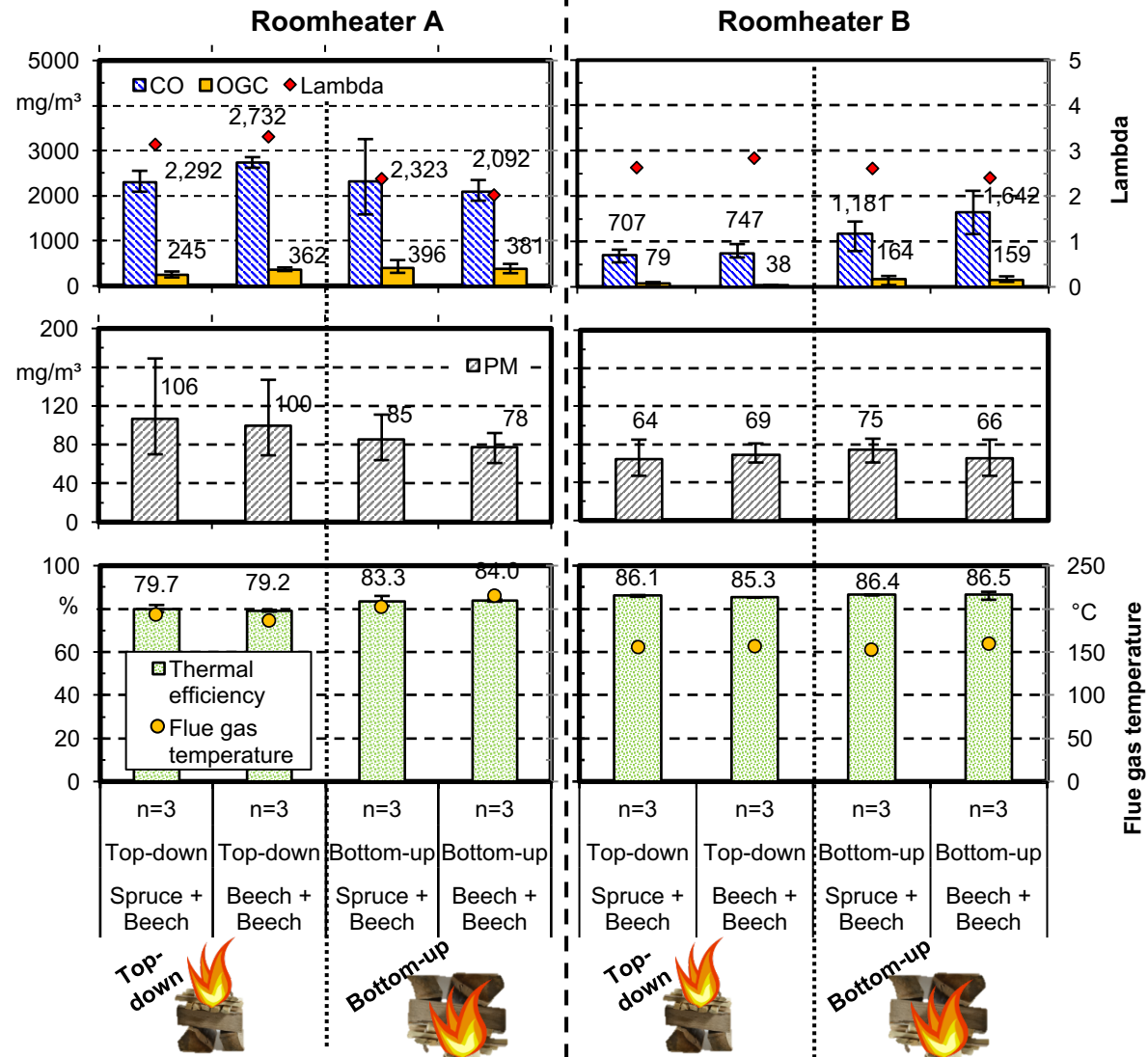
Bottom-up ignition mode less CO and PM emissions

- CO: ~ 12% / PM: ~ 20%
- BUT: Lowest OGC emissions achieved by top-down ignition

Roomheater B:

Lower CO and OGC emissions for top-down ignition mode

- CO: ~ 50% / OGC: ~ 65%
- PM: only marginal differences
- Best thermal efficiencies achieved by bottom-up ignition mode
- Ignition mode is an **obligatory** part of the **Quick-User-Guide**

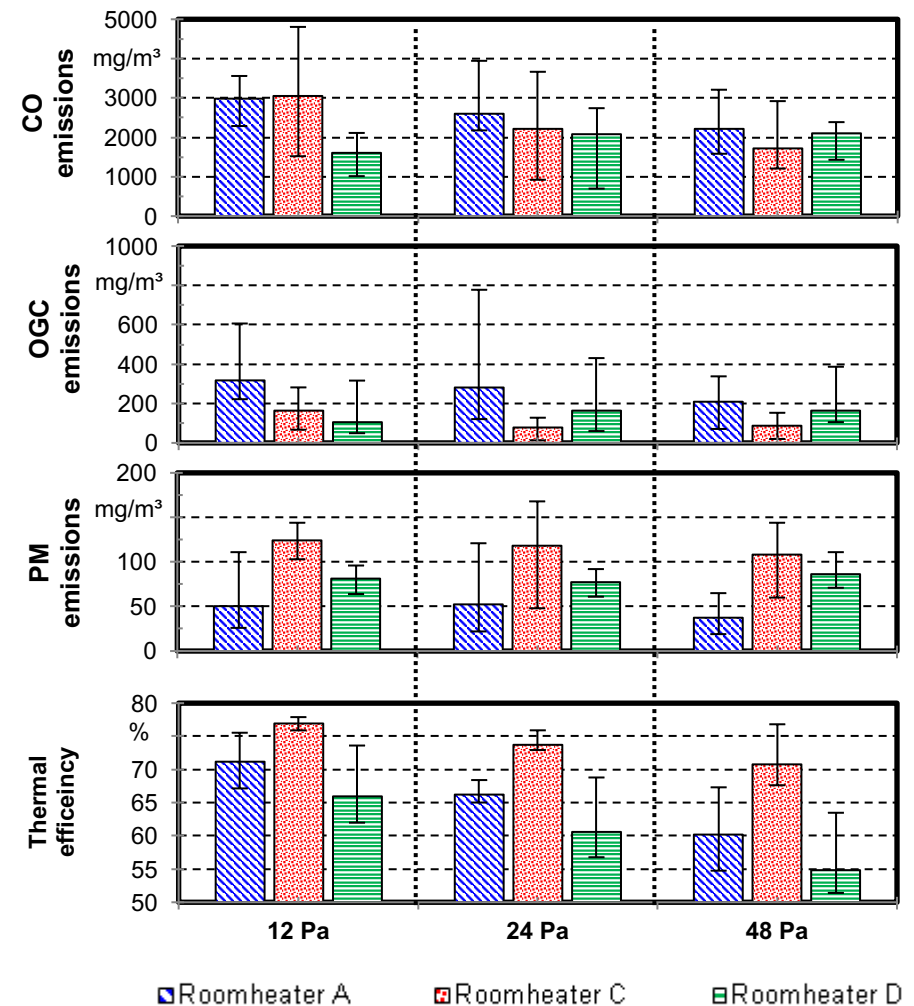


- all emission concentrations in mg/m³, at STP conditions, dry, transferred to 13 vol.-% O₂

Firewood Stoves

Effect of draught conditions

- Trends of impact of increased draught on CO & OGC were investigated (but: statistically not significant)
 - Stove A & C: Emissions **decreased**
 - Stove D: Emissions **increased**
- **Correlation** of draught conditions and gaseous emission depend on the **appliance specifics**
- No effect of draught conditions on PM emissions → **no correlation**
- **Decrease of thermal efficiency** at higher draught level for all three roomheaters → **Correlation statistically significant**
- **Higher draught** conditions result in **lower thermal efficiency**



- all emission concentrations in mg/m³, at STP conditions, dry, transferred to 13 vol.-% O₂

Providing **insights & highlights** of the **development process** of the „beReal“ methods for firewood and pellet stoves

Pellet Stoves*

- Fuel quality: A screening on pellet quality from Europe
 - Pellet quality and combustion performance
- Effect of cleaning process on emissions and thermal efficiency

Motivation

- Varying qualities of wood pellets & search for suitable test fuels for pellet stoves

Approach

- Pellets considered in screening: Wood pellets in bags/ 42 samples in total
 - 20 samples from Germany, 22 samples from all over Europe (Austria, Switzerland, Sweden, France, Estonia, Denmark, UK, Belgium, Poland, Czech Republic, Italy)
 - Quality label: 27 with EN_{plus}, 22 with DIN_{plus}, 8 samples without label
 - Some pellet samples from different factories but same producer



Analysis program

- Combustion properties: Ash & moisture content, net calorific value
- Physical properties: Bulk density, mechanical durability, share of fines
- Chemical composition: Nitrogen, sulfur, chlorine content, ash forming elements

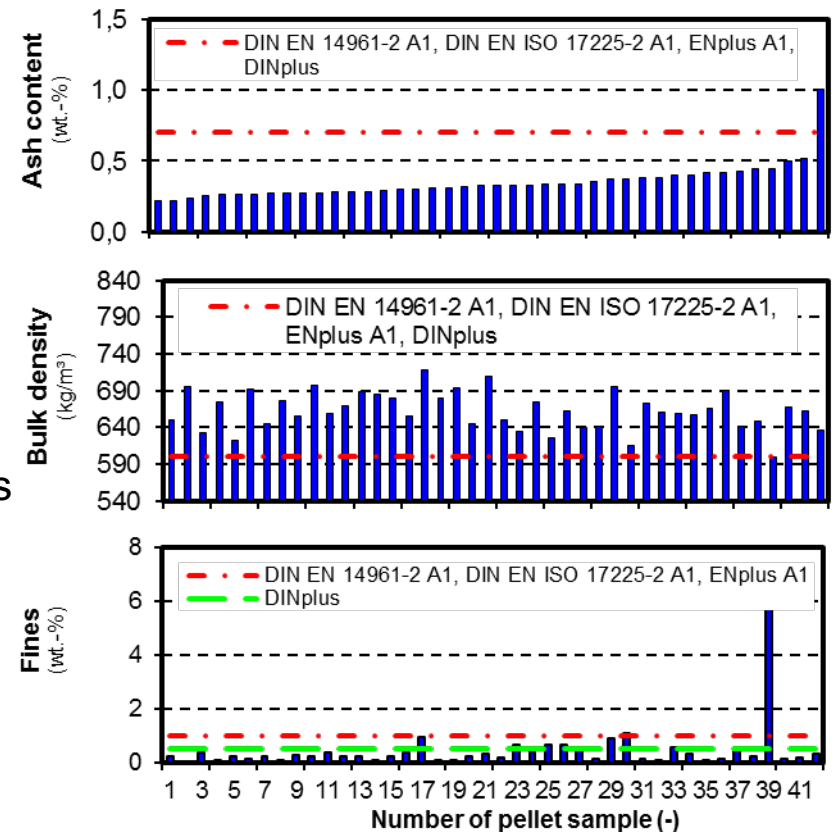
Results

Combustion properties:

- **Ash content:** All samples with increasing ash content (@ 550°C); Only one sample (# 42) does not fulfil requirements of A1 quality
- **Moisture content:** Only one sample (# 39) does not fulfil requirements of A1 quality (<10%)
- **Net calorific value:** All samples fulfil the requirements regarding net calorific value (Ø 18,956 kJ/kg_{d.b.})

Physical properties:

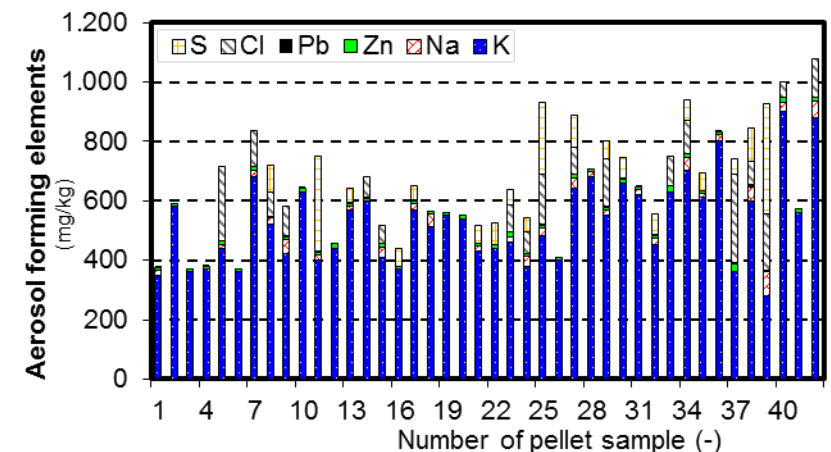
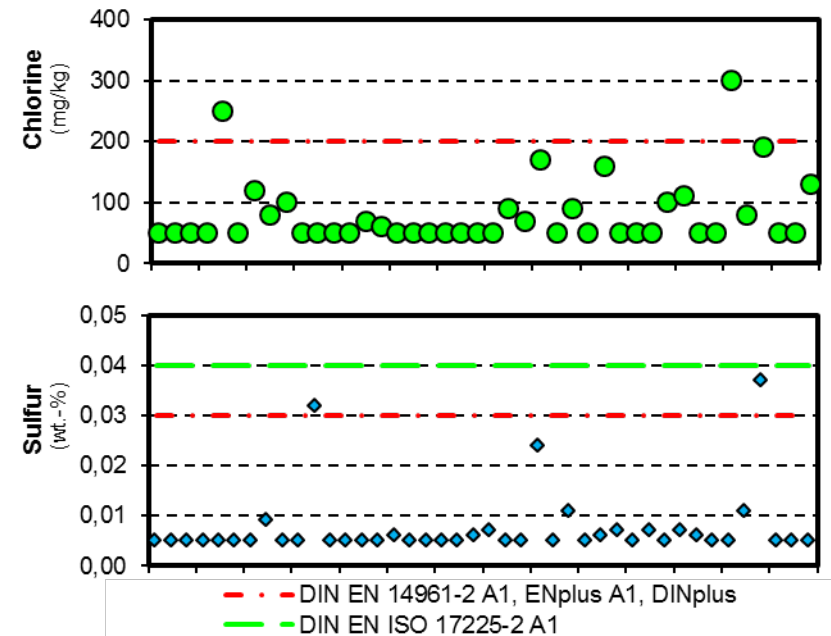
- **Bulk density:** Only one pellet sample does not meet the requirements but is very close to the value (599 versus 600 kg/m³). Average bulk density of 662 kg/m³ (range: 599 to 717 kg/m³)
- **Mechanical durability:** Two samples do not meet the requirement of > 97.5 (# 23 and # 39)
- **Share of fines:** DIN_{plus} has stricter limits on fines for bagged pellets compared to EN_{plus} and ISO. Two samples do not meet the ISO-requirements (# 30 and # 39)



Results

Chemical composition:

- **Nitrogen content**
 - All samples meet the requirements on nitrogen content (DIN EN ISO 17225-2 A1 & EN_{plus}: < 0.3 wt.-%).
 - **Sulfur content**
 - All samples meet the new ISO standard. Lower values for certified pellets
 - **Chlorine content**
 - Two samples exceed the limiting values of 0.02 wt.-% (# 5 and # 37)
 - **Aerosol forming elements**
 - Aerosol forming elements are dominated by K content (280 - 900 mg/kg; Ø 528 mg/kg)
- **Positive results for quality** of wood pellets on the German and European market



Motivation

- Impact of different fuel characteristics during operation in one conventional pellet stove (8 kW)

Approach

- Serial combustion of 12 selected pellet fuels from the pellet screening
- 3 PM samples, each over 15 minutes per fuel, using plane filters
- All 12 selected fuels are EN_{plus}-certified wood pellets

After preheating the pellet stove for at least 1 hour

1.

Refilling the storage tank with the next fuel → 15 min to burn the previous fuel completely



2.

Execution of 3 PM samples with a duration of 15 min per sample



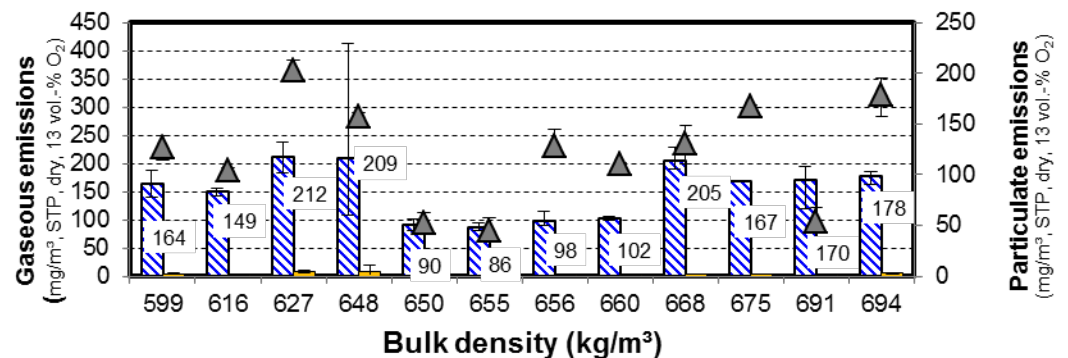
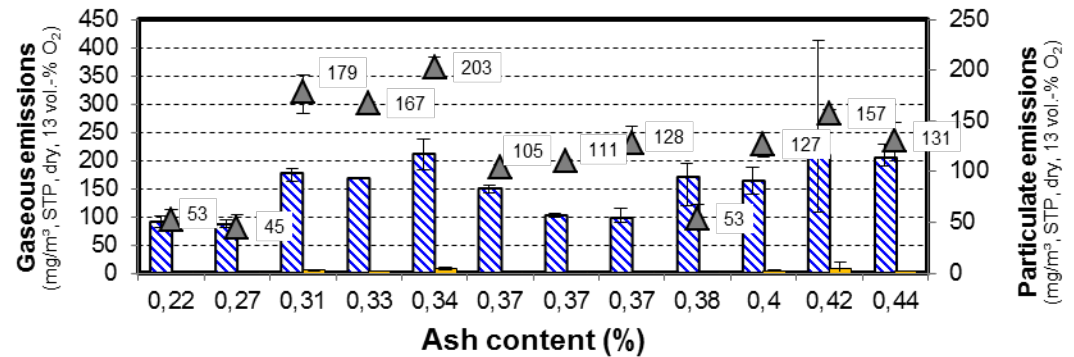
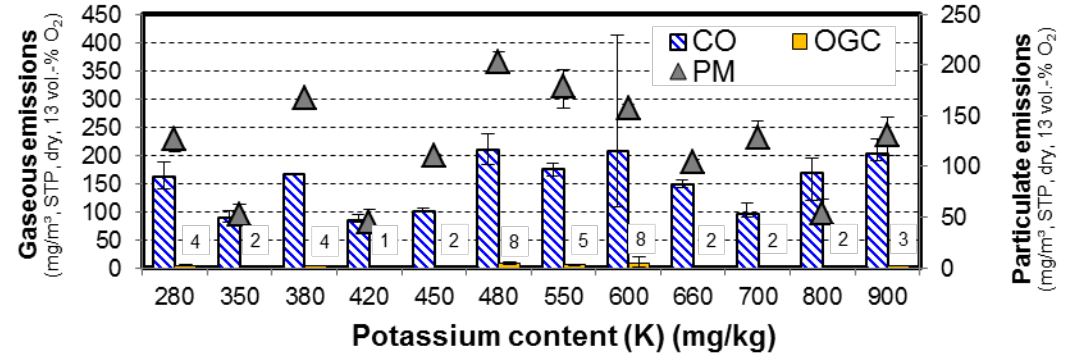
3.

Cleaning the storage tank and the stoker screw completely with a vacuum cleaner



Results

- Different EN_{plus}-certified pellets can cause **very large emission variations** with one pellet room heater.
- There is **no clear trend** showing the emissions as function of **ash content**, **potassium content**, **bulk density** etc.
- Multiple regression analyses has brought no further knowledge (many more testing replications would be required).
- Yet unknown pellet properties need to be investigated
- Picking up the best suitable fuel can lead to big advantages
- beReal: Test fuel has to be provided by the testing institute

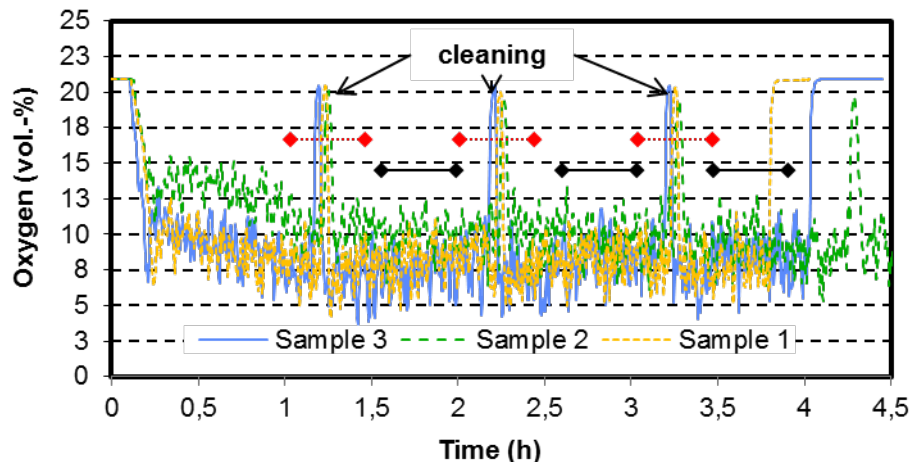





Motivation

- Impact of **cleaning process** on combustion performance

Approach

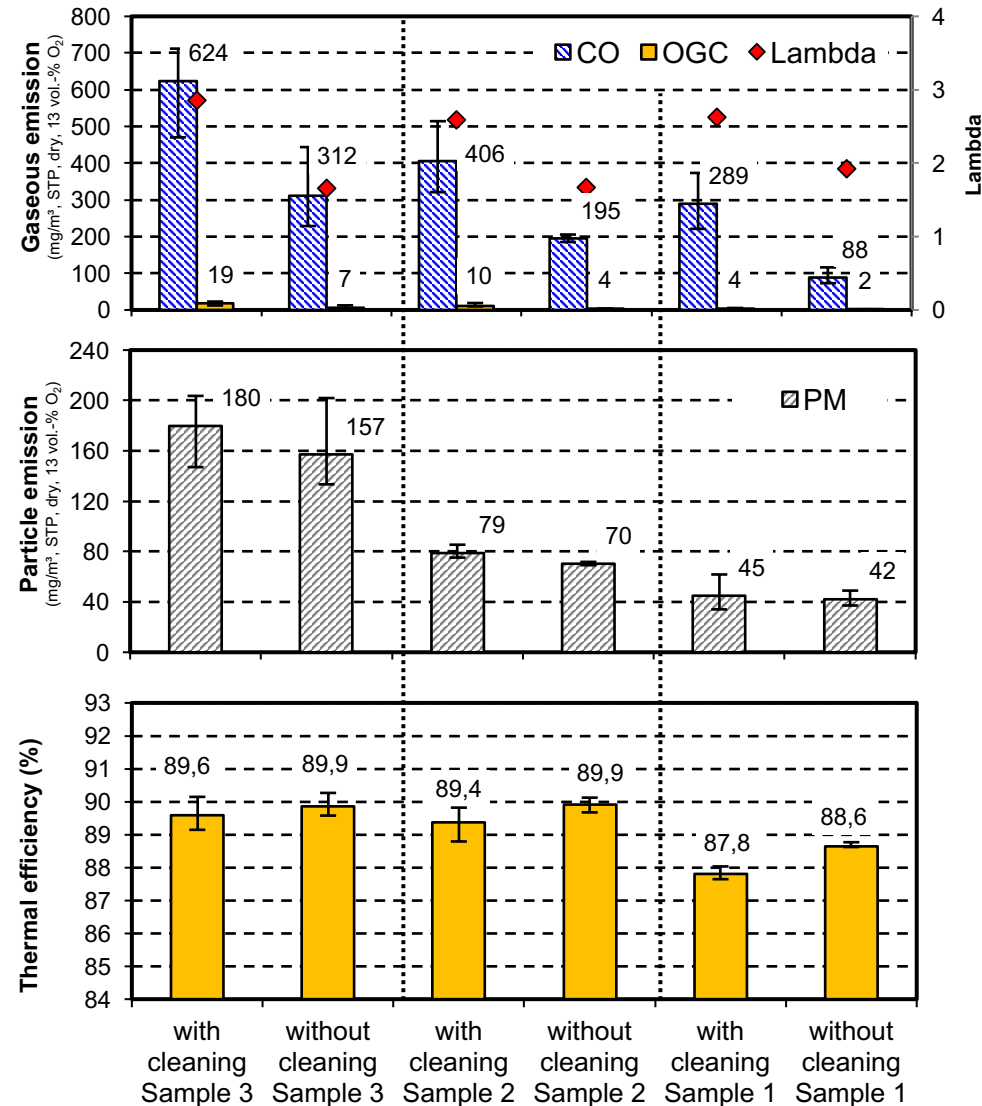
- Evaluation of gaseous and particulate emissions **with** (◆-----◆) and **without** (◄-----►) the cleaning interval (30 min)
- Tests were carried out with three different pellet samples (Sample 1 – 3)
- One commercial pellet stove (EN 14785) was used (Nominal load: 8 kW)



Number of Sample	1	2	3
			
Producing country	Austria	Belgium	Poland
Certification	EN Plus A1	DIN Plus	-
Description	wood pellets	pinewood without bark	100 % wood
Diameter [mm]	6	6	6
Heating value [kJ/kg]	18790	18893	19330
Ash content [%]	0.26	0.28	0.33
Moisture content [%]	7.3	7.4	3.3
Bulk density [kg/m ³]	622	669	709
Mechanical strength [%]	98.9	99.2	98.9
Fines [%]	0.25	0.24	0.33
C [Ma.-%]	51.0	50.1	51.3
H [Ma.-%]	6.1	6.1	6.2
O [Ma.-%]	42.8	43.7	42.4
N [Ma.-%]	0.10	0.09	0.10
S [Ma.-%]	0.005	0.005	0.006
S [mg/kg]	<5	<5	6
Cl [mg/kg]	250	<50	<50
K [mg/kg]	440	440	430
Na [mg/kg]	13	<10	17
Zn [mg/kg]	10	15	9
Sum of aerosol formers [mg/kg]	718	520	512

Results

- **Different emissions** for the three fuel samples (same finding compared to the previous test series in another stove)
- **Gaseous emissions “with cleaning” significantly higher** compared to “without cleaning” for gaseous emissions
- Average **PM emissions lower** for intervals “without cleaning” compared to “with cleaning”
- **Lower thermal efficiency** when the cleaning process is considered, but: In general, the effect of the cleaning process on thermal efficiency was low
- **Cleaning phase** has to be **considered** in the beReal test method. The cleaning interval was included in the testing and data evaluation of beReal



Acknowledgements

Associations



Company partners



Subcontractor



Acknowledgements

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Thanks for listening !

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